

# → TRANSMISSION LINE PARAMETER

## ⇒ TRANSMISSION LINES :-

• The transform the energy from one point to another take place through either the transmission lines is wave guides

• The electrical lines which are used to transmitted. The electrical wave to one place to another place.

• Example of transmission line

i) Telephone cable

ii) Electrical power signal

## ⇒ TYPES OF TRANSMISSION LINES :-

### 1) OPEN WIRE LINE :-

It is made of Aluminium and copper. It is not insulated with any material.

Ex.

i) Telephone line

ii) Electrical power signal line.

### 2) CABLES :-

These are under ground line. These wire are insulated by plastic or paper.

### 3) Co-axial Cables :-

It has two conductor one conductor is hollow and other is place co-axially inside in 1<sup>st</sup> conductor.

#### 4) WAVE GUIDES :-

This are used to transmitted by micro wave frequency (range 1 GHz to 300 GHz)

#### \* TRANSMISSION LINE PARAMETER

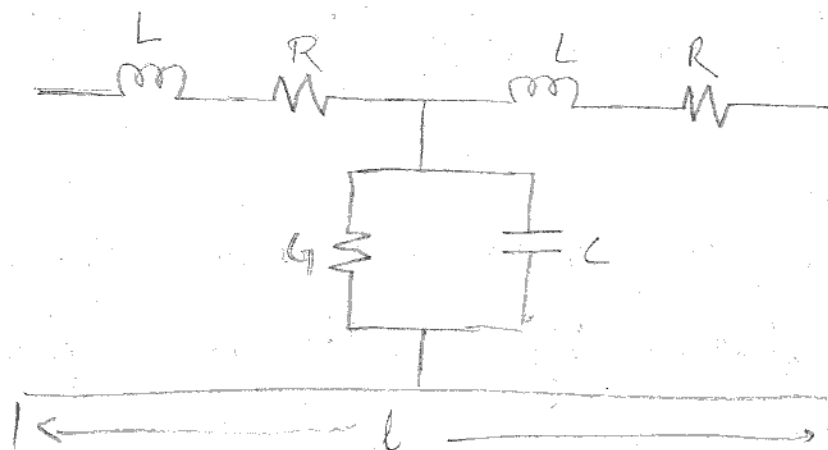
- i) Resistance (R)
- ii) Capacitance (C)
- iii) Inductance (L)
- iv) Conductance (G)

#### \* CHARACTERISTIC IMPEDANCE ( $Z_0$ ) :-

- Characteristic impedance symmetrical network is the impedance is measured at the input of the first network in the chain of infinite network in cascade.

#### \* EQUIVALENT IN CIRCUIT OF TRANSMISSION

LINE :-



- The parameter  $R$ ,  $L$ ,  $C$  &  $G$  are distributed throu out the transmission

lines. The series impedance of transmission lines is represented by  $Z$

$$\Rightarrow Z = R + j\omega L$$

where

$\omega$  - freq. of the line

The shunt admittance

$$\Rightarrow Y = G + j\omega C$$

$$\Rightarrow Z_1 = (R + j\omega L) l$$

$$\Rightarrow Y_1 = (G + j\omega C) l$$

we know that

$$\Rightarrow Z = \frac{1}{Y}$$

$$Z_2 = \frac{1}{Y_1} = \frac{1}{(G + j\omega C) l}$$

characteristic impedance of total m/w

$$\Rightarrow Z_0 = \sqrt{\frac{Z_1^2}{4} + Z_1 Z_2} \quad \text{--- (1)}$$

$$\Rightarrow = \sqrt{\frac{(R + j\omega L)^2 l^2}{4} + (R + j\omega L) l \cdot \frac{1}{(G + j\omega C) l}}$$

$$\Rightarrow = \sqrt{\frac{(R + j\omega L)^2 l^2}{4} + \frac{(R + j\omega L)}{(G + j\omega C)}}$$

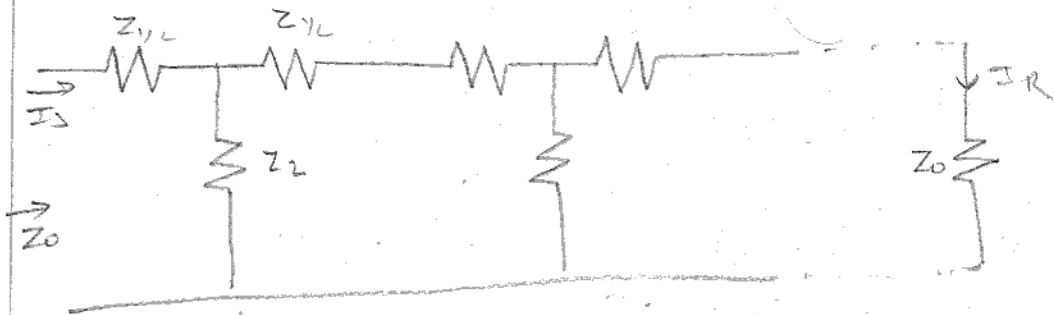
Let us assume length is very short  
substitute the value  $l = 0$

$$\Rightarrow Z_0 = \frac{\sqrt{R + j\omega L}}{\sqrt{G + j\omega C}} = \sqrt{\frac{Z}{Y}}$$

$$\Rightarrow Z_0 = \sqrt{\frac{Z}{Y}}$$

# \* TRANSMISSION LINE AS CASCADED

T section →



- $I_s \Rightarrow$  sending current
- $I_R \Rightarrow$  Receiving current.

$$\Rightarrow \boxed{I_s = I_R e^{nD}} \quad \text{gamma}$$

$$\text{Sending current} = I_R e^{nD}$$

where  $n$  is no. of network

- $D$  is propagation constant

$$\Rightarrow \boxed{D = \alpha + i\beta}$$

- $\alpha$  is attenuation (lost)
- $\beta$  is phase shift

\* The receiving current at first network

$$\Rightarrow I_1 = I_s \times \frac{Z_2}{Z_{1/2} + Z_0 + Z_2}$$

$$\Rightarrow \frac{I_s}{I_1} = \frac{Z_{1/2} + Z_0 + Z_2}{Z_2}$$

We know that

$$\Rightarrow \frac{I_s}{I_R} = e^{nD}$$

for 1<sup>st</sup> network

$$\Rightarrow \frac{I_s}{I_1} = e^{\nu}$$

$$\Rightarrow e^{\nu} = 1 + \frac{Z_0}{Z_2} + \frac{Z_{1/2}}{Z_2}$$

$$\Rightarrow \frac{I_1}{I_2} = e^{\nu} = 1 + \frac{Z_0}{Z_2} + \frac{Z_{1/2}}{Z_2}$$

$$\Rightarrow \frac{I_s}{I_2} = \frac{I_s}{I_1} \times \frac{I_1}{I_2} = e^{2\nu}$$

$$\Rightarrow \boxed{\frac{I_s}{I_R} = e^{n\nu}}$$

### \* PROPAGATION CONSTANT ( $\nu$ ) $\Rightarrow$

Propogation Constant is defines is the natural logarithmic the ratio of sending end current or voltage receiving end current or voltage.

$$\Rightarrow \nu = \ln \frac{I_s}{I_R} \quad \text{or} \quad \ln \frac{V_s}{V_R}$$

$$\Rightarrow \nu = \alpha + j\beta$$

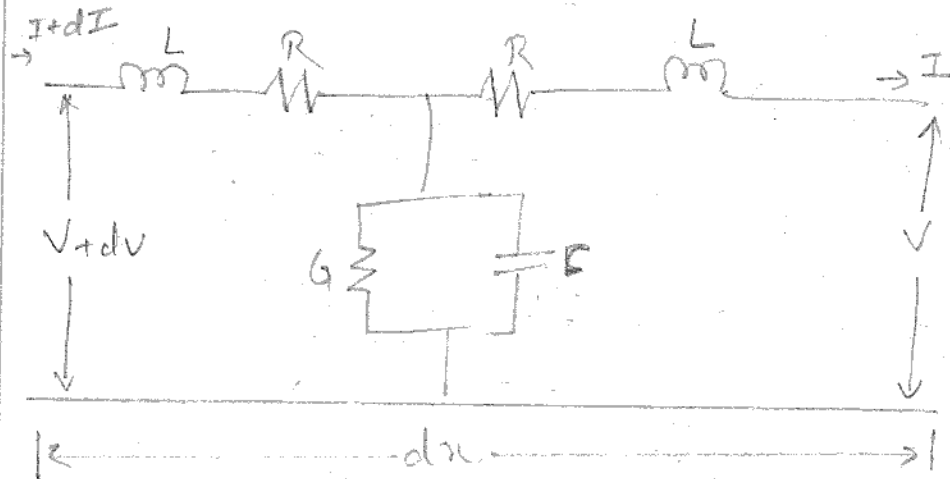
also known as

$$\Rightarrow \nu = \sqrt{ZY}$$

$$\Rightarrow \nu = \sqrt{(R + j\omega L)(G + j\omega C)}$$

# The General Solution Of Transmission

Line (Tr. line eq.) :-



- Let assume the current line  $I + dI$
- $L, R, C$  &  $G$  are trans. line parameters.
- The series impedance of the trans. line

$$\Rightarrow Z = (R + j\omega L)$$

- The shunt admittance of the trans. line

$$\Rightarrow Y = (G + j\omega C)$$

- Consider the trans. line is having some distance. This distance is represent as  $dx$ . The impedance is

$$\Rightarrow Z = (R + j\omega L) dx$$

and shunt admittance is

$$\Rightarrow Y = (G + j\omega C) dx$$

- Consider  $V + dv$  is i/p voltage of the trans. line and  $I + dI$  is input current of the trans. line.

- $V, I$  is the output voltage & current of the trans. line.
- The potential (voltage) difference b/w two end (i/p into o/p).

$$\Rightarrow V + dV - V = I (R + j\omega L) dx$$

$$\Rightarrow \frac{dV}{dx} = I (R + j\omega L)$$

$$\Rightarrow \boxed{\frac{dV}{dx} = I Z} \text{ ————— } \textcircled{1}$$

- The current difference in i/p end into output end.

$$\Rightarrow I + dI - I = V (G + j\omega C) dx$$

$$\Rightarrow \boxed{\frac{dI}{dx} = V Y} \text{ ————— } \textcircled{2}$$

- Diff. eq<sup>n</sup>  $\textcircled{1}$  with respect to  $x$

$$\Rightarrow \frac{d^2 I}{dx^2} = (R + j\omega L) \frac{dI}{dx}$$

$$\Rightarrow \boxed{\frac{d^2 I}{dx^2} = (R + j\omega L)(G + j\omega C) V} \text{ ————— } \textcircled{3} \text{ [} \because \text{ from eq<sup>n</sup> 2]} \text{ ]}$$

- Similarly diff. eq<sup>n</sup>  $\textcircled{2}$  with r. to  $x$

$$\Rightarrow \frac{d^2 V}{dx^2} = (G + j\omega C) \frac{dV}{dx}$$

$$\Rightarrow \boxed{\frac{d^2 V}{dx^2} = (G + j\omega C)(R + j\omega L) I} \text{ ————— } \textcircled{4} \text{ [} \because \text{ from eq<sup>n</sup> 1]} \text{ ]}$$

- We already know that the propagation gamma constant

$$\Rightarrow \gamma = \sqrt{(R + j\omega L)(G + j\omega C)}$$

→ The potential (voltage) difference b/w two end (i/p into o/p).

$$\Rightarrow V + dV - V = I (R + j\omega L) dx$$

$$\Rightarrow \frac{dV}{dx} = I (R + j\omega L)$$

$$\Rightarrow \boxed{\frac{dV}{dx} = I Z} \text{ ————— } \textcircled{1}$$

→ The current difference in i/p end into output end.

$$\Rightarrow I + dI - I = V (G + j\omega C) dx$$

$$\Rightarrow \boxed{\frac{dI}{dx} = V Y} \text{ ————— } \textcircled{2}$$

→ Diff. eq<sup>n</sup> ① with respect to  $x$

$$\Rightarrow \frac{d^2 I}{dx^2} = (R + j\omega L) \frac{dI}{dx}$$

$$\Rightarrow \boxed{\frac{d^2 I}{dx^2} = (R + j\omega L) (G + j\omega C) V} \text{ ————— } \textcircled{3} \text{ [} \because \text{ from eq<sup>n</sup> 2]} \text{ ]}$$

→ Similarly diff. eq<sup>n</sup> ② with r. to  $x$

$$\Rightarrow \frac{d^2 V}{dx^2} = (G + j\omega C) \frac{dV}{dx}$$

$$\Rightarrow \boxed{\frac{d^2 V}{dx^2} = (G + j\omega C) (R + j\omega L) I} \text{ ————— } \textcircled{4} \text{ [} \because \text{ from eq<sup>n</sup> 1]} \text{ ]}$$

→ We already know that the propagation gamma constant

$$\Rightarrow \gamma = \sqrt{(R + j\omega L) (G + j\omega C)}$$

$$\Rightarrow \gamma = \sqrt{ZY}$$



Sub. the value of gamma in eq<sup>n</sup> (3) & eq<sup>n</sup> (4)

$$\left\{ \therefore \text{Let } \frac{d^2V}{dx^2} = m = \frac{d^2I}{dx^2} \right\}$$

$$\frac{d^2V}{dx^2} = \nu^2 V$$

$$(m^2 - \nu^2)V = 0$$

$$m = \pm \nu$$

$$\frac{d^2I}{dx^2} = \nu^2 I$$

$$(m^2 - \nu^2)I = 0$$

$$m = \pm \nu$$

$$V = A e^{\nu x} + B e^{-\nu x} \quad \text{--- (5)}$$

$$I = C e^{\nu x} + D e^{-\nu x} \quad \text{--- (6)}$$

where

A, B, C & D is an arbitrary constant

Diff. eq<sup>n</sup> (5) w.r. to x

$$\frac{dV}{dx} = A \nu e^{\nu x} - B \nu e^{-\nu x}$$

from eq<sup>n</sup> (6)  $\frac{dV}{dx} = I \nu Z$

$$I Z = A \nu e^{\nu x} - B \nu e^{-\nu x}$$

$$\left\{ \therefore \nu = \sqrt{ZY} \right\}$$

$$I Z = A \sqrt{ZY} e^{\sqrt{ZY} x} - \nu \sqrt{ZY} e^{-\sqrt{ZY} x}$$

$$I = A \sqrt{\frac{Y}{Z}} e^{\sqrt{ZY} x} - B \sqrt{\frac{Y}{Z}} e^{-\sqrt{ZY} x} \quad \text{--- (7)}$$

Similarly diff. eq<sup>n</sup> (6) w.r.t. to  $x$

$$\frac{dI}{dx} = C \nu e^{\nu x} - D \nu e^{-\nu x}$$

$$V = C \sqrt{\frac{z}{y}} e^{\sqrt{\frac{z}{y}} x} - D \sqrt{\frac{z}{y}} e^{-\sqrt{\frac{z}{y}} x} \quad \text{--- (8)}$$

If the trans. line is short  $x=0$   
and replace the value  $I = I_R$ ,  $V = V_R$

This condition applying to eq<sup>n</sup> (5) & (6)

$$V_R = A + B \quad \text{--- (9)}$$

$$I_R = C + D \quad \text{--- (10)}$$

$$\left. \begin{array}{l} \text{Let } x=0 \\ e^{\nu x} = e^0 = 1 \end{array} \right\}$$

Some condition should apply eq<sup>n</sup> (7) & (8)

$$I_R = A \sqrt{\frac{y}{z}} - B \sqrt{\frac{y}{z}} \quad \text{--- (11)}$$

$$V_R = C \sqrt{\frac{z}{y}} - D \sqrt{\frac{z}{y}} \quad \text{--- (12)}$$

Let us assume  $\sqrt{\frac{z}{y}} = x$

$$\frac{1}{x} = \sqrt{\frac{y}{z}}$$

rep

$$I_R = \frac{A}{x} - \frac{B}{x} = \frac{1}{x} (A - B)$$

Compare above eq<sup>n</sup> with eq<sup>n</sup> (10)

$$C + D = \frac{1}{x} (A - B)$$

$$Cx + Dx = A - B \quad \text{--- (13)}$$

Similarly

$$V = Cx - Dx$$

$$\frac{dI}{dx} = C \sqrt{z/y} e^{\sqrt{z/y} x} - D \sqrt{z/y} e^{-\sqrt{z/y} x}$$

$$V = C \sqrt{z/y} e^{\sqrt{z/y} x} - D \sqrt{z/y} e^{-\sqrt{z/y} x} \quad \text{--- (8)}$$

If the trans. line is short  $x=0$   
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$$\frac{1}{x} = \sqrt{y/z}$$

sep

$$I_R = \frac{A}{x} - \frac{B}{x} = \frac{1}{x} (A - B)$$

Compare above eq<sup>n</sup> with eq<sup>n</sup> (10)

$$C + D = \frac{1}{x} (A - B)$$

$$Cx + Dx = A - B \quad \text{--- (13)}$$

Similarly

$$V_R = Cx - Dx$$

→ Compare above eq<sup>n</sup> with eq<sup>n</sup> (9)

$$\Rightarrow \boxed{A+B = Cx - Dx} \text{--- (14)}$$

$$\Rightarrow \boxed{A-B = Cx + Dx}$$

→ adding eq<sup>n</sup> (13) and (14)

$$\Rightarrow 2A = 2Cx$$

$$\Rightarrow A = Cx$$

→ Subtracting eq<sup>n</sup> (13) and (14)

$$\Rightarrow 2B = -2Dx$$

$$\Rightarrow B = -Dx$$

→ Sub: the value of A & B in eq<sup>n</sup> (9)

$$\Rightarrow \boxed{V_R = Cx - Dx} \text{--- (15)}$$

• from (10)

$$\Rightarrow I_R = C + D$$

→ multiplying by x in eq<sup>n</sup> (10)

$$\Rightarrow \boxed{I_R x = Cx + Dx} \text{--- (16)}$$

→ Should +ve add eq<sup>n</sup> (15) and (16)

$$\Rightarrow V_R + I_R x = 2Cx$$

$$\Rightarrow C = \frac{I_R}{2} + \frac{V_R}{2x}$$

$$\Rightarrow \boxed{C = \frac{I_R}{2} + \frac{V_R}{2} \sqrt{1/Z}} \text{--- (17)}$$

→ Subtracting the eq<sup>n</sup> (15) and (16)

$$\Rightarrow V_R - I_R x = -2Dx$$

$$\Rightarrow 2Dx = I_R x - V_R$$

$$\Rightarrow A + B = Cx - Dx \quad \text{--- (14)}$$

$$\Rightarrow A - B = Cx + Dx$$

→ adding eq<sup>n</sup> (13) and (14)

$$\Rightarrow 2A = 2Cx$$

$$\Rightarrow A = Cx$$

→ Subtracting eq<sup>n</sup> (13) and (14)

$$\Rightarrow 2B = -2Dx$$

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→ Sub: the value of A & B in eq<sup>n</sup> (9)

$$\Rightarrow V_R = Cx - Dx \quad \text{--- (15)}$$

• from (10)

$$\Rightarrow I_R = C + D$$

→ multiplying by x in eq<sup>n</sup> (11)

$$\Rightarrow I_R x = Cx + Dx \quad \text{--- (16)}$$

→ Should we add eq<sup>n</sup> (15) and (16)

$$\Rightarrow V_R + I_R x = 2Cx$$

$$\Rightarrow C = \frac{I_R}{2} + \frac{V_R}{2x}$$

$$\Rightarrow C = \frac{I_R}{2} + \frac{V_R}{2} \sqrt{1/Z} \quad \text{--- (17)}$$

→ Subtracting the eq<sup>n</sup> (15) and (16)

$$\Rightarrow V_R - I_R x = -2Dx$$

$$\Rightarrow 2Dx = I_R x - V_R$$

$$\Rightarrow D = \frac{I_R}{2} - \frac{V_R}{2} \sqrt{1/Z} \quad \text{--- (18)}$$

$$\Rightarrow A = Cx$$

$$\Rightarrow A = \frac{I_R}{2} + \frac{V_R}{2x} \cdot x$$

$$\Rightarrow \boxed{A = \frac{V_R}{2} + \frac{V_R}{2} \sqrt{z/y}} \quad \text{--- (19)}$$

$$\Rightarrow B = -Dx$$

$$\Rightarrow B = -\frac{I_R x}{2} + \frac{V_R}{2x} \cdot x$$

$$\Rightarrow \boxed{B = \frac{V_R}{2} - \frac{I_R}{2} \sqrt{z/y}} \quad \text{--- (20)}$$

• The characteristic impedent

$$\Rightarrow Z_0 = \sqrt{z/y}$$

• from ohm's law

$$\Rightarrow V_R = I_R Z_L \quad , \quad I_R = \frac{V_R}{Z_R}$$

$$\Rightarrow Z_0 = \sqrt{z/y}$$

$$\Rightarrow A = \frac{V_R}{2} + \frac{I_R}{2} \sqrt{z/y}$$

$$\Rightarrow = \frac{V_R}{2} + \frac{V_R}{2Z_R} \cdot Z_0 \quad \left\{ \because I_R = \frac{V_R}{Z_R} \right\}$$

$$\Rightarrow \boxed{A = \frac{V_R}{2} \left( 1 + \frac{Z_0}{Z_R} \right)} \quad \text{--- (21)}$$

$$\Rightarrow B = \frac{V_R}{2} - \frac{I_R}{2} \sqrt{z/y}$$

$$\Rightarrow \boxed{B = \frac{V_R}{2} \left( 1 - \frac{Z_0}{Z_R} \right)} \quad \text{--- (22)}$$

$$\Rightarrow C = \frac{I_R}{2} + \frac{V_R}{2} \sqrt{y/z}$$

$$\Rightarrow C = \frac{I_R}{2} + \frac{I_R Z_R}{2Z_0} \quad \left\{ \because V_R = I_R Z_R \right\}$$

$$\Rightarrow \boxed{C = \frac{I_R}{2} \left( 1 + \frac{Z_R}{Z_0} \right)} \quad \text{--- (23)}$$

$$\Rightarrow D = \frac{I_R}{2} \left( 1 - \frac{Z_R}{Z_0} \right) \quad \text{--- (24)}$$

• Substitute the value of A, B, C, D in eq<sup>n</sup> (5) & (6)

$$\Rightarrow V = \frac{V_R}{2} \left( 1 + \frac{Z_0}{Z_R} \right) e^{\gamma x} + \frac{V_R}{2} \left( 1 - \frac{Z_0}{Z_R} \right) e^{-\gamma x} \quad \text{--- (25)}$$

$$\Rightarrow I = \frac{I_R}{2} \left( 1 + \frac{Z_R}{Z_0} \right) e^{\gamma x} + \frac{I_R}{2} \left( 1 - \frac{Z_R}{Z_0} \right) e^{-\gamma x} \quad \text{--- (26)}$$

• from eq<sup>n</sup> (25)

$$\Rightarrow V = \frac{V_R}{2} e^{\sqrt{\gamma} x} + \frac{V_R}{2} \frac{Z_0}{Z_R} e^{\sqrt{\gamma} x} + \frac{V_R}{2} e^{-\sqrt{\gamma} x} - \frac{V_R}{2} \frac{Z_0}{Z_R} e^{-\sqrt{\gamma} x}$$

$$\Rightarrow V = \frac{V_R}{2} \left[ \frac{e^{\sqrt{\gamma} x} + e^{-\sqrt{\gamma} x}}{2} \right] + I_R Z_0 \left[ \frac{e^{\sqrt{\gamma} x} - e^{-\sqrt{\gamma} x}}{2} \right]$$

$$\left\{ \because V_R = I_R Z_R \right\}$$

$$\Rightarrow V = V_R \cosh \sqrt{\gamma} x + \frac{I_R}{2} Z_0 \sinh \sqrt{\gamma} x \quad \text{--- (27)}$$

• from eq<sup>n</sup> (26)

$$\Rightarrow I = \frac{I_R}{2} e^{\sqrt{\gamma} x} + \frac{I_R}{2} \frac{Z_R}{Z_0} e^{\sqrt{\gamma} x} + \frac{I_R}{2} e^{-\sqrt{\gamma} x} - \frac{I_R}{2} \frac{Z_R}{Z_0} e^{-\sqrt{\gamma} x}$$

$$\Rightarrow I = V_R \cosh \sqrt{\gamma} x + \frac{V_R}{Z_0} \sinh \sqrt{\gamma} x \quad \text{--- (28)}$$

⇒ eq<sup>n</sup> (27) & (28) are general solution of transmission lines.

# THE PHYSICAL SIGNIFICANCE OF GENERAL

Sol<sup>n</sup> :-

SENDING IMPEDENCE :-

It is the ratio of sending voltage  
& sending current

$$Z_s = \frac{V_s}{I_s}$$

$$V_s = V_R \cosh \gamma l + I_R Z_0 \sinh \gamma l$$

$$I_s = I_R \cosh \gamma l + \frac{V_R}{Z_0} \sinh \gamma l$$

$V_R$  is replace by  $I_R Z_R$

$$V_s = I_R Z_R \cosh \gamma l + I_R Z_0 \sinh \gamma l$$

$$I_s = I_R \cosh \gamma l + \frac{I_R Z_R}{Z_0} \sinh \gamma l$$

dividing above equ

$$Z_s = Z_0 \left[ \frac{Z_R \cosh \gamma l + Z_0 \sinh \gamma l}{Z_0 \cosh \gamma l + Z_R \sinh \gamma l} \right]$$

Condition I<sup>st</sup> :-

When the line is terminated the  $Z_R = Z_0$

$$Z_s = Z_0 \left[ \frac{Z_0 \cosh \gamma l + Z_0 \sinh \gamma l}{Z_0 \cosh \gamma l + Z_0 \sinh \gamma l} \right] \quad [Z_R = Z_0]$$

$$\Rightarrow \boxed{Z_s = Z_0}$$

Condition II<sup>nd</sup> :-

The trans. line is infinite length here

$$l = \infty$$



$$Z_s = Z_0 \frac{\cosh \gamma l \left[ Z_R + \frac{Z_0 \sinh \gamma l}{\cosh \gamma l} \right]}{\cosh \gamma l \left[ Z_0 + \frac{Z_R \sinh \gamma l}{\cosh \gamma l} \right]}$$

$$= Z_0 \frac{Z_R + Z_0 \tanh \gamma l}{Z_0 + Z_R \tanh \gamma l}$$

Put  $l = \infty$

$$= Z_0 \frac{Z_R + Z_0 \tanh \infty}{Z_0 + Z_R \tanh \infty}$$

$$= Z_0 \frac{Z_R + Z_0}{Z_0 + Z_R}$$

$$\boxed{Z_s = Z_0}$$

## REFLECTION CO-EFFICIENT

This is depends as the ratio of reflected voltage to the incident voltage (i.e. voltage) at the receiving end denote by  $K$

$$K = \frac{\text{Reflected voltage}}{\text{incident voltage}} = \frac{V_R}{V_s}$$

The general voltage eq<sup>n</sup> of trans. line from eq<sup>n</sup> (25)

$$V = \frac{V_R}{2} \left[ \left(1 + \frac{Z_0}{Z_R}\right) e^{\gamma x} + \left(1 - \frac{Z_0}{Z_R}\right) e^{-\gamma x} \right]$$

$$= \frac{V_R}{2} \left[ \left( \frac{Z_R + Z_0}{Z_R} \right) e^{j\beta x} + \left( \frac{Z_R - Z_0}{Z_R} \right) e^{-j\beta x} \right]$$

$$V = \frac{V_R}{2} \frac{Z_R + Z_0}{Z_R} e^{j\beta x} + \frac{V_R}{2} \frac{Z_R - Z_0}{Z_R} e^{-j\beta x}$$

The first term  $e^{j\beta x}$  is represent the "incident wave".

The second term  $e^{-j\beta x}$  is represent the "reflected wave".

$$K = \frac{\frac{V_R}{2} \frac{Z_R - Z_0}{Z_R}}{\frac{V_R}{2} \frac{Z_R + Z_0}{Z_R}}$$

$$= \frac{Z_R - Z_0}{Z_R + Z_0}$$

It is also defined as in the terms of the ratio of reflected current to the incident current. But it is negative

$$K = \frac{-I_R}{I_s}$$

If the trans. line is terminated by characteristic impedance  $Z_R = Z_0$  at that time reflected co-efficient become zero.

$$\lambda = v/f$$

## WAVE LENGTH

The distance traveled by the wave along the line which the <sup>fall</sup> phase angle is changing through  $2\pi R$  is called wave length.

$$\beta \lambda = 2\pi$$

$$\lambda = \frac{2\pi}{\beta}$$

$$\beta = \frac{2\pi}{\lambda}$$

## VELOCITY PROPAGATION

We know that the propagation gamma constant is equal to

$$\Rightarrow \gamma = \sqrt{ZY}$$

$$\Rightarrow \gamma = \sqrt{(R + j\omega L)(G + j\omega C)}$$

squaring both side

$$\Rightarrow \gamma^2 = (R + j\omega L)(G + j\omega C)$$

$$\Rightarrow \gamma^2 = RG + Rj\omega L + jG\omega L - \omega^2 LC$$

$$\Rightarrow \gamma^2 = (RG - \omega^2 LC) + j\omega(RC + GL)$$

Condition 1<sup>st</sup>  $\Rightarrow$

Here minimum attenuation in 'L'

$$L = \frac{RC}{G}$$

$$LG = RC$$

$$\gamma^2 = (RG - \omega^2 LC) + 2j\omega RC$$

$$\gamma^2 = RG - \omega^2 LC + j2\omega \sqrt{RCLG}$$

$$\gamma^2 = (\sqrt{RG} + j\omega\sqrt{LC})^2$$

$$\gamma = \sqrt{RG + j\omega\sqrt{LC}}$$

$$\alpha = \sqrt{RG}$$

$$\beta = \omega\sqrt{LC}$$

$$\gamma = \alpha + j\beta$$

The velocity propagation is given by

$$V = \lambda f$$

multiple and divided by  $2\pi$

$$V = \frac{\lambda}{2\pi} 2\pi f$$

$$= \frac{1}{\beta} \omega$$

$$V = \frac{\omega}{\beta} = \frac{\omega}{\omega\sqrt{LC}}$$

$$V = \frac{1}{\sqrt{LC}}$$

22/6/11

### DISTORTION LINE

When the receiving signal is always having noise in this received signal is called as distorted line.

It has two types.

- i) Freq. distortion line
- ii) Phase " "

### 1) FREQUENCY DISTORTION LINE

Frequency distortion due to the variation of attenuation constant  $\alpha$

$$\alpha = \frac{\sqrt{RG - \omega^2 LC} + \sqrt{(RG - \omega^2 LC)^2 + \omega^2 (LG + RC)^2}}{2}$$

## 2) PHASE DISTORTION LINE :-

It is due to the variation of phase constant  $\beta$ .

$$\beta = \sqrt{\frac{1}{2V} \sqrt{(R^2 + \omega^2 L^2)(G^2 + \omega^2 C^2) - (RG - \omega^2 LC)}}$$

## DISTORTION LESS LINE :-

A line in which there is no phase and frequency distortion. It is known as distortion less line.

Condition 1<sup>st</sup> :-

It always represent by  $\beta$

$$\Rightarrow \beta = \sqrt{\omega^2 LC - RG + \sqrt{(RG - \omega^2 LC)^2 + \omega^2 (LG + RC)^2}} \\ = (\omega^2 LC + RG)^2$$

If the transmission line is distortion less line the second term is

$$\Rightarrow (RG - \omega^2 LC)^2 + \omega^2 (LG + RC)^2 = (\omega^2 LC + RG)^2$$

$$\Rightarrow R^2 G^2 + \omega^4 L^2 C^2 - 2RG\omega^2 LC + \omega^2 L^2 G^2 + R^2 C^2 \omega^2 + 2\omega^2 LGRC \\ = \omega^4 L^2 C^2 + R^2 G^2 + 2\omega^2 LC RG$$

$$\Rightarrow \omega^2 L^2 G^2 + \omega^2 R^2 C^2 - 2RG\omega^2 LC = 0$$

$$\Rightarrow \omega^2 (LG - RC)^2 = 0$$

$$\Rightarrow LG - RC = 0$$

$$\Rightarrow LG = RC$$

$$\Rightarrow \boxed{\frac{G}{C} = \frac{R}{L}}$$

TELEPHONE CABLE  
 It is line insulated with plastic or paper - this construction result - the negligible value of inductance and conductance ( $L \& G$ ).

CONDITION FOR TELEPHONE CABLE :-

$L\omega$  is very much less than resistance

$$\boxed{L\omega \ll R}$$

$$\& \boxed{G \ll C\omega}$$

So the impedance  $Z$  is equal to  $R + j\omega L$

$$Z = R + j\omega L = R$$

The admittance

$$Y = G + j\omega C \approx j\omega C$$

The propagation constant of telephone cable.

$$\begin{aligned} D &= \sqrt{ZY} = \sqrt{j\omega RC} = \sqrt{\omega RC} \angle 90^\circ \\ &= \sqrt{\omega RC} \angle 45^\circ = \sqrt{\omega RC} (\cos 45^\circ + j \sin 45^\circ) \\ &= \sqrt{\omega RC} \frac{1}{\sqrt{2}} + j \frac{1}{\sqrt{2}} \\ &= \sqrt{\omega RC} \frac{1}{\sqrt{2}} (1 + j) \\ &= \sqrt{\frac{\omega RC}{2}} + j \sqrt{\frac{\omega RC}{2}} \end{aligned}$$

already we know that

$$D = \alpha + j\beta$$

$$\alpha = \sqrt{\frac{\omega RC}{2}} \quad \beta = \sqrt{\frac{\omega RC}{2}}$$

The velocity of propagation of telephone cable

$$V = \omega / \beta = \frac{\omega}{\sqrt{\frac{\omega RC}{2}}} = \frac{\sqrt{\omega} \sqrt{\omega}}{\sqrt{\frac{\omega RC}{2}}} = \sqrt{\frac{2\omega}{RC}}$$

characteristic impedance of  
telephone cable.

$$Z_0 = \sqrt{Z/Y}$$

$$Z_0 = \sqrt{R/j\omega c}$$

$$Z_0 = \sqrt{\frac{R \angle -90^\circ}{\omega c}}$$

$$Z_0 = \sqrt{\frac{R}{\omega c}} \angle -45^\circ$$